第二讲 图像采集



周文晖

计算机学院

计算机视觉的问题



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几何成像模型

- •像机与场景坐标系间的映射关系
 - •小孔成像模型
 - •射影几何(投影几何)
 - 灭点和灭线(Vanishing points and lines)
 - •投影矩阵

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2.1 成像模型

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小孔成像



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小孔像机——早期像机(暗室)

- •古中国和古希腊就已被发现和提出
- •中国春秋时期墨子的《墨经》是世界上最早对几何光学进行系统论述的典籍。



Illustration of Camera Obscura



Freestanding camera obscura at UNC Chapel Hill

Photo by Seth Ilys

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小孔像机的孔径选择

•若孔径太大,多个方向光照平均后,造成图像模糊。



•若孔径太小,衍射效应会导致图像模糊。



2 mm







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第一个带透镜的像机暗箱

•1568年意大利Daniel Barbaro(丹尼尔巴尔巴洛)《远近实际方法》。采用了凸透镜。



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保留至今的最早像片,铅锡合金板上经8小时曝光





法国 Joseph Niepce, 1826

收藏在美国得克萨斯大学收藏馆

1839年,法国Louis Daguerre(达盖尔)发明"银版摄影技术",人 类史上第一个成功的发明摄影技术,命名为"达盖尔照相术"。

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- 主平面特性
 - •a) 主平面位置没有任何约束
 - •b) 主平面间无平移变换

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景深:弥散圆(circle of confusion)

- •光线射入凸透镜后,汇聚到焦点上
- •在焦点前后,光线开始聚集和扩散,点的影象变模糊,形成一个扩大的圆,这个圆就叫做弥散圆。



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景深: 容许弥散圆

- 若弥散圆的直径小于人眼的鉴别能力,即在一定范围内实际影象产生的模糊是不能辨认的。
 这个不能辨认的弥散圆就称为容许弥散圆。
- 在焦点前后各有一个容许弥散圆,

这两个弥散圆之间的距离就叫景深。



景深 △L

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焦深

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景深: 焦距与光圈值

- •景深随镜头的焦距、光圈值、拍摄距离而变化。
- •固定焦距和拍摄距离,使用光圈越小,景深越大。







f/5.6

f/32

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2.2 投影过程

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射影几何:长度信息丢失

- 哪些物理信息丢失?
 - •长度



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射影几何:长度信息丢失



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射影几何:角度信息丢失

- •还有哪些物理信息丢失?
 - 角度



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射影几何:具有不变特性的属性

- 有哪些物理信息得以保持?
 - 直线特性
 - 交比不变性



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灭点(Vanishing point)和灭线

•场景中的平行线投影到图像平面后,会聚于"灭点"



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2.3 投影矩阵

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成像过程:透视投影

• 三维场景 → 二维图像



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齐次坐标

笛卡尔坐标 → 齐次坐标



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齐次坐标

•尺度不变性



齐次坐标 笛卡尔坐标

▶ 笛卡尔坐标表示一个点对应于齐次坐标表示一条直线
▶ w = 1称为标准齐次坐标

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透视投影中坐标系转换

• 透视投影: 世界坐标 → 图像坐标

•之前基于像机坐标系的推导没意义?

- 三类坐标系间转换(笛卡尔坐标系)
 - •世界坐标系: XYZ
 - •像机坐标系: xyz
 - •图像坐标系: uv



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像机坐标系与世界坐标系间转换



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•像机坐标系原点在世界坐标系下的坐标为(t_x, t_y, t_z)



平移矩阵:



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- •像机坐标系旋转过程分为三步:
 - •像机坐标系绕世界坐标系X轴旋转角度 θ_x (偏转角)
 - •像机坐标系绕世界坐标系Y轴旋转角度 θ_v (俯仰角)
 - •像机坐标系绕世界坐标系Z轴旋转角度 θ_z (侧倾角)

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旋转矩阵: 绕Y轴旋转



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$$\mathbf{R}_{x} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta_{x} & -\sin \theta_{x} \\ 0 & \sin \theta_{x} & \cos \theta_{x} \end{bmatrix} \qquad \mathbf{R}_{z} = \begin{bmatrix} \cos \theta_{z} & -\sin \theta_{z} & 0 \\ \sin \theta_{z} & \cos \theta_{z} & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

旋转矩阵:

 $\mathbf{R}_{3\times 3} = \mathbf{R}_{z}\mathbf{R}_{y}\mathbf{R}_{x}$

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$$\mathbf{R} = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} = \mathbf{R}_{z} \mathbf{R}_{y} \mathbf{R}_{x}$$

$$= \begin{bmatrix} \cos \theta_{z} & -\sin \theta_{z} & 0 \\ \sin \theta_{z} & \cos \theta_{z} & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos \theta_{y} & 0 & \sin \theta_{y} \\ 0 & 1 & 0 \\ -\sin \theta_{y} & 0 & \cos \theta_{y} \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta_{x} & -\sin \theta_{x} \\ 0 & \sin \theta_{x} & \cos \theta_{x} \end{bmatrix}$$

$$= \begin{bmatrix} \cos \theta_{y} \cos \theta_{z} & -\sin \theta_{z} & \sin \theta_{y} \cos \theta_{z} \\ \cos \theta_{y} \sin \theta_{z} & \cos \theta_{z} & \sin \theta_{y} \sin \theta_{z} \\ -\sin \theta_{y} & 0 & \cos \theta_{y} \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta_{x} & -\sin \theta_{x} \\ 0 & \sin \theta_{x} & \cos \theta_{x} \end{bmatrix}$$

$$= \begin{bmatrix} \cos \theta_{y} \cos \theta_{z} & \sin \theta_{x} \sin \theta_{y} \cos \theta_{z} - \cos \theta_{x} \sin \theta_{z} & \cos \theta_{x} \\ -\sin \theta_{y} & 0 & \cos \theta_{z} - \cos \theta_{x} \sin \theta_{z} & \cos \theta_{x} \end{bmatrix}$$

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旋转矩阵的约束条件

$$\mathbf{R} = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix}$$

R的9个参数应满足6个约束:

 $\mathbf{RR'} = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} \begin{bmatrix} r_{11} & r_{21} & r_{31} \\ r_{12} & r_{22} & r_{32} \\ r_{13} & r_{23} & r_{33} \end{bmatrix} = \mathbf{I}$

$$\begin{cases} r_{11}^{2} + r_{12}^{2} + r_{13}^{2} = 1 \\ r_{21}^{2} + r_{22}^{2} + r_{23}^{2} = 1 \\ r_{31}^{2} + r_{32}^{2} + r_{33}^{2} = 1 \\ r_{11}r_{21}^{2} + r_{12}r_{22}^{2} + r_{13}r_{23} = 0 \\ r_{11}r_{31}^{2} + r_{12}r_{32}^{2} + r_{13}r_{33} = 0 \\ \hline r_{21}r_{11}^{2} + r_{22}r_{12}^{2} + r_{23}r_{13} = 0 \\ \hline r_{21}r_{31}^{2} + r_{22}r_{32}^{2} + r_{23}r_{33} = 0 \\ \hline r_{31}r_{11}^{2} + r_{32}r_{12}^{2} + r_{33}r_{13} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{32}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{21}^{2} + r_{32}r_{22}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{32}^{2} + r_{33}r_{23} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{32}^{2} + r_{33}r_{33} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{32}^{2} + r_{33}r_{33} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{32}^{2} + r_{33}r_{33}^{2} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{32}^{2} + r_{33}r_{33}^{2} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{32}^{2} + r_{33}r_{33}^{2} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{32}^{2} + r_{33}r_{33}^{2} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{32}^{2} + r_{33}r_{33}^{2} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{32}^{2} + r_{33}r_{33}^{2} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{32}^{2} + r_{33}r_{33}^{2} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{31}^{2} + r_{33}r_{31}^{2} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{31}^{2} + r_{33}r_{31}^{2} = 0 \\ \hline r_{31}r_{31}^{2} + r_{32}r_{31}^{2} + r_{31}r_{31}^{2} + r_{32}r_{31}^{2} + r_{33}r_{31}^{2} = 0 \\ \hline r_{31}r_$$

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旋转矩阵的约束条件

• R为正交矩阵

$$\mathbf{RR'} = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} \begin{bmatrix} r_{11} & r_{21} & r_{31} \\ r_{12} & r_{22} & r_{32} \\ r_{13} & r_{23} & r_{33} \end{bmatrix} = \mathbf{I}$$

• 有

 $\mathbf{R}^{-1}=\mathbf{R'}$

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像机坐标系与图像坐标系间转换

•通常图像坐标系uv平面与像机坐标系xoy平面平行



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像机坐标系与图像坐标系的一般化形式

- •实际CCD/CMOS传感器u轴和v轴可能会不垂直
- •图像坐标系 u-c-v, u轴v轴夹角为 θ
- •像机坐标系在图像平面的投影 x'-O_c-y'

$$\begin{cases} u_p = \frac{x'_p - y'_p \cot \theta}{dx} + u_0 \\ v_p = \frac{y'_p / \sin \theta}{dy} + v_0 \end{cases}$$



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$$\begin{cases} u_p = \frac{x'_p - y'_p \cot \theta}{dx} + u_0 \\ v_p = \frac{y'_p / \sin \theta}{dy} + v_0 \end{cases}$$



$$\begin{bmatrix} u_p \\ v_p \\ 1 \end{bmatrix} = \begin{bmatrix} 1/dx & -\cot\theta/dx & u_0 \\ 0 & 1/(dy \cdot \sin\theta) & v_0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x'_p \\ y'_p \\ 1 \end{bmatrix}$$

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$$z_{p} \begin{bmatrix} u_{p} \\ v_{p} \\ 1 \end{bmatrix} = \begin{bmatrix} 1/dx & 0 & u_{0} \\ 0 & 1/dy & v_{0} \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} f & 0 & 0 & | & 0 \\ 0 & f & 0 & | & 0 \\ 0 & 0 & 1 & | & 0 \end{bmatrix} \begin{bmatrix} \mathbf{R}_{3\times3} & \mathbf{T}_{3\times1} \\ \mathbf{0}_{3\times1}^{T} & 1 \end{bmatrix} \begin{bmatrix} X_{p} \\ Y_{p} \\ Z_{p} \\ 1 \end{bmatrix}$$
$$\int f_{x} = f/dx \\ f_{y} = f/dy$$
$$z_{p} \begin{bmatrix} u \\ v \\ 1 \end{bmatrix} = \begin{bmatrix} f_{x} & 0 & u_{0} & | & 0 \\ 0 & f_{y} & v_{0} & | & 0 \\ 0 & 0 & 1 & | & 0 \end{bmatrix} \begin{bmatrix} \mathbf{R}_{3\times3} & \mathbf{T}_{3\times1} \\ \mathbf{0}_{3\times1}^{T} & 1 \end{bmatrix} \begin{bmatrix} X \\ Y \\ Z \\ 1 \end{bmatrix}$$

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$$z_{p} \begin{bmatrix} u_{p} \\ v_{p} \\ 1 \end{bmatrix} = \begin{bmatrix} 1/dx & -\cot\theta/dx & u_{0} \\ 0 & 1/(dy \cdot \sin\theta) & v_{0} \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} f & 0 & 0 & | & 0 \\ 0 & f & 0 & | & 0 \\ 0 & 0 & 1 & | & 0 \end{bmatrix} \begin{bmatrix} \mathbf{R}_{3\times3} & \mathbf{T}_{3\times1} \\ \mathbf{0}_{3\times1}^{T} & 1 \end{bmatrix} \begin{bmatrix} X_{p} \\ Y_{p} \\ Z_{p} \\ 1 \end{bmatrix}$$
$$f_{x} = f/dx$$
$$f_{y} = f/(\sin\theta \cdot dy)$$
$$\gamma = -f \cot\theta/dx$$
$$z_{p} \begin{bmatrix} u \\ v \\ 1 \end{bmatrix} = \begin{bmatrix} f_{x} & \gamma & u_{0} & | & 0 \\ 0 & f_{y} & v_{0} & | & 0 \\ 0 & 0 & 1 & | & 0 \end{bmatrix} \begin{bmatrix} \mathbf{R}_{3\times3} & \mathbf{T}_{3\times1} \\ \mathbf{0}_{3\times1}^{T} & 1 \end{bmatrix} \begin{bmatrix} X \\ Y \\ Z \\ 1 \end{bmatrix}$$

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像机内参和外参:一般化形式

像机内部参数像机外部参数(内参)(外参)



y表示u轴和v轴的不垂直因子。

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像机内参和外参说明

- 像机内参
 - • f_x : u轴尺度因子,或称u轴归一化焦距
 - f_v : v轴尺度因子,或称v轴归一化焦距
 - *γ*: *u*轴和*v*轴的不垂直因子,通常为0
 - *u*₀, *v*₀: 光学中心
- 像机外参
 - R: 像机旋转矩阵
 - •T: 像机平移矩阵

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第二讲 图像采集

2.4 像机标定

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像机标定问题

•目的:确定像机的内参和外参。

$$z_{p}\begin{bmatrix} u \\ v \\ 1 \end{bmatrix} = \begin{bmatrix} f_{x} & \gamma & u_{0} & | & 0 \\ 0 & f_{y} & v_{0} & | & 0 \\ 0 & 0 & 1 & | & 0 \end{bmatrix} \begin{bmatrix} \mathbf{R}_{3\times 3} & \mathbf{T}_{3\times 1} \\ \mathbf{0}_{3\times 1}^{T} & 1 \end{bmatrix} \begin{bmatrix} X \\ Y \\ Z \\ 1 \end{bmatrix}$$

- •思路:通过一组已知世界坐标的图像特征点,建立 超定方程求解。
- •方法:最小二乘求解超定方程,寻找最优估计。

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• 给定n个世界坐标已知的场景点 P_i , $i \in [1,n]$, 并已知它们投影在图像上的投影点坐标。

•建立超定方程组,并最优求解。

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像机参数自由度分析



至少需要多少个已知场景点才能估计出像机参数?

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2.4.1 线性模型像机标定

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线性模型像机标定

• 直接线性变换(DLT变换): 求解投影矩阵

• 投影矩阵
$$\mathbf{M}_{3\times4} = \begin{bmatrix} m'_{11} & m'_{12} & m'_{13} & m'_{14} \\ m'_{21} & m'_{22} & m'_{23} & m'_{24} \\ m'_{31} & m'_{32} & m'_{33} & m'_{34} \end{bmatrix} = \begin{bmatrix} \alpha_x & \gamma & u_0 & | & 0 \\ 0 & \alpha_y & v_0 & | & 0 \\ 0 & 0 & 1 & | & 0 \end{bmatrix} \begin{bmatrix} \mathbf{R}_{3\times3} & \mathbf{T}_{3\times1} \\ \mathbf{0}_{3\times1}^T & 1 \end{bmatrix}$$

• 线性模型的齐次方程表示

$$z_{p}\begin{bmatrix} u\\v\\1\end{bmatrix} = \mathbf{M}_{3\times 4}\begin{bmatrix} X\\Y\\Z\\1\end{bmatrix}$$

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线性模型像机标定:投影矩阵

$$z_{p}\begin{bmatrix} u \\ v \\ 1 \end{bmatrix} = \begin{bmatrix} m_{11} & m_{12} & m_{13} & m_{14} \\ m_{21} & m_{22} & m_{23} & m_{24} \\ m_{31} & m_{32} & m_{33} & m_{34} \end{bmatrix} \begin{bmatrix} X \\ Y \\ Z \\ 1 \end{bmatrix}$$
$$m_{34} \ddagger 5 \mathsf{R} \mathsf{E} \boxdot \mathsf{F} \qquad \mathbf{11} \mathsf{C} \triangleq \mathsf{B} \oiint$$
$$z_{p}'\begin{bmatrix} u \\ v \\ 1 \end{bmatrix} = \begin{bmatrix} m_{11} & m_{12} & m_{13} & m_{14} \\ m_{21} & m_{22} & m_{23} & m_{24} \\ m_{31} & m_{32} & m_{33} & 1 \end{bmatrix} \begin{bmatrix} X \\ Y \\ Z \\ 1 \end{bmatrix}; \qquad z_{p}' = \frac{z_{p}}{m_{34}}$$

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线性模型像机标定

• 已知场景点P的世界坐标为(X_i, Y_i, Z_i),其在图像上投影点坐标为(u_i, v_i).

$$\begin{cases} z'_{i}u_{i} = m_{11}X_{i} + m_{12}Y_{i} + m_{13}Z_{i} + m_{14} \\ z'_{i}v_{i} = m_{21}X_{i} + m_{22}Y_{i} + m_{23}Z_{i} + m_{24} \\ z'_{i} = m_{31}X_{i} + m_{32}Y_{i} + m_{33}Z_{i} + 1 \end{cases}$$

$$\ddot{\mu} Rc_{z'}$$

$$\begin{cases} m_{11}X_i + m_{12}Y_i + m_{13}Z_i + m_{14} - u_i m_{31}X_i - u_i m_{32}Y_i - u_i m_{33}Z_i = u_i \\ m_{21}X_i + m_{22}Y_i + m_{23}Z_i + m_{24} - v_i m_{31}X_i - v_i m_{32}Y_i - v_i m_{33}Z_i = v_i \end{cases}$$

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线性模型像机标定

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常性模型像机标定: n个已知场景点
求解超定线性方程组
$$\begin{bmatrix}
X_1 Y_1 Z_1 1 0 0 0 0 -u_1 X_1 -u_1 Y_1 -u_1 Z_1 \\
0 0 0 0 X_1 Y_1 Z_1 1 -v_1 X_1 -v_1 Y_1 -v_1 Z_1 \\
... \\
X_n Y_n Z_n 1 0 0 0 0 -u_n X_n -u_n Y_n -u_n Z_n \\
0 0 0 0 X_n Y_n Z_n 1 -v_n X_n -v_n Y_n -v_n Z_n
\end{bmatrix}
\begin{bmatrix}
u_1 \\
m_{12} \\
m_{13} \\
m_{14} \\
m_{21} \\
m_{22} \\
m_{23} \\
m_{24} \\
m_{31} \\
m_{32} \\
m_{33}
\end{bmatrix}$$

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第二讲 图像采集

2.4.1 非线性模型像机标定

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径向畸变和切向畸变



•将图像坐标转为极坐标表示。

• dr为极坐标的幅度变化量,表现为径向畸变。

• dt为极坐标的角度变化量,表现为切向畸变。

在大多数视觉应用中切向畸变通常很小,因此
 可忽略。

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径向畸变

• 径向畸变的修正量由距图像中心(u0,v0)的径向距离的偶次幂多项式模型来表示。

$$\begin{cases} \delta_x = x'_d \left(k_1 r^2 + k_2 r^4 + ... \right) \\ \delta_y = y'_d \left(k_1 r^2 + k_2 r^4 + ... \right) \end{cases}$$

• 其中

$$r^2 = \left(x'_d\right)^2 + \left(y'_d\right)^2$$

• 对一般视觉应用,只需考虑一阶径向畸变

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像机非线性模型的参数

- 内部参数
 - •线性模型参数 a_x , a_y , u_0 , v_0
 - •非线性模型参数 k_1 , k_2
- 外部参数
 - •旋转矩阵 R

•平移矩阵**T** =
$$(t_x, t_y, t_z)$$

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基于径向约束的像机标定

- Roger Tsai 1987年提出基于径向约束的两步法标定
 - •第一步:利用径向一致性约束,求解旋转矩阵**R**,平移矩阵 **T**的 t_x , t_y 分量及尺度因子 s_x
 - •第二步:求解焦距f,平移矩阵 \mathbf{T} 的 t_z 分量和径向畸变参数 k_1

(只考虑一阶径向畸变)

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径向排列约束RAC(Radial Alignment Constraint)

- 像机坐标系下:
 - •实际像点 P_d 坐标 (x'_d, y'_d)
 - •理想像点 P_u 坐标 (x'_u, y'_u)
- •实际像点 P_d 图像坐标 (u_d, v_d)
- 径向畸变不改变方向,即 O_R - P_d - P_u 共线。
- RAC约束: $O_R P_d / P_{oz} P_w$

$$\frac{x'_d}{y'_d} = \frac{x'_u}{y'_u} = \frac{x}{y}$$



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图像坐标与传感器坐标转换

$$\begin{bmatrix} u_d \\ v_d \\ 1 \end{bmatrix} = \begin{bmatrix} 1/dx & 0 & u_0 \\ 0 & 1/dy & v_0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x'_d \\ y'_d \\ 1 \end{bmatrix} \Rightarrow \begin{bmatrix} u_d - u_0 \\ v_d - v_0 \end{bmatrix} = \begin{bmatrix} 1/dx & 0 \\ 0 & 1/dy \end{bmatrix} \begin{bmatrix} x'_d \\ y'_d \end{bmatrix}$$

dx, dy为像素在x'和y'方向的物理尺寸

dx, dy如何获得?

传感器输出的

- 1)图像像素水平间距(水平采样)与传感单元水平间距通常无直接关联;
- 2) 图像像素垂直方向采样受传感单元垂直间距限制;
- 3) 像素水平尺寸和垂直尺寸比例(图像像素尺度因子或称纵横比)未知

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图像坐标与传感器坐标转换

 $dx = d_x N_{cx} / f_{cx}$ $d_x x$ 方向(扫描线方向)相邻传感单元中心间距 $N_{cx} x$ 方向传感单元的个数

 f_{cx} x方向的图像像素个数

 $dy = d_y$ d_y y方向(扫描线方向)相邻传感单元中心间距

s_x 图像像素尺度因子或称纵横比

$$\begin{bmatrix} u_d - u_0 \\ v_d - v_0 \end{bmatrix} = \begin{bmatrix} s_x/dx & 0 \\ 0 & 1/dy \end{bmatrix} \begin{bmatrix} x'_d \\ y'_d \end{bmatrix} \Longrightarrow \frac{x'_d}{y'_d} = \frac{1}{s_x} \frac{(u - u_0)d_x N_{cx}/f_{cx}}{(v - v_0)d_y} \xrightarrow{\frac{x'_d - (u - u_0)d_x N_{cx}/f_{cx}}{\frac{x'_d - (v - v_0)d_y}{\frac{x'_d - (v - v_0)d_y}{$$

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径向排列约束 (RAC)

由像机坐标系与世界坐标系间的关系式



根据RAC约束, 有
$$\frac{x'_d}{y'_d} = \frac{x}{y} = \frac{r_{11}X_w + r_{12}Y_w + r_{13}Z_w + t_x}{r_{21}X_w + r_{22}Y_w + r_{23}Z_w + t_y}$$

即: $\frac{x''_d}{y''_d} = \frac{s_x r_{11}X_w + s_x r_{12}Y_w + s_x r_{13}Z_w + s_x t_x}{r_{21}X_w + r_{22}Y_w + r_{23}Z_w + t_y}$

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 y_d

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径向排列约束 (RAC)

•
$$\Leftrightarrow$$
 $a_1 = s_x r_{11}/t_y; a_2 = s_x r_{12}/t_y; a_3 = s_x r_{13}/t_y; a_4 = s_x t_x/t_y$
 $a_5 = r_{21}/t_y; a_6 = r_{22}/t_y; a_7 = r_{23}/t_y$

• 基于RAC约束的参数求解方程简写为:

$$\begin{bmatrix} X_w y''_d & Y_w y''_d & Z_w y''_d & y''_d & -X_w x''_d & -Y_w x''_d & -Z_w x''_d \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \\ a_5 \\ a_6 \\ a_7 \end{bmatrix} = x''_d$$

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•利用径向一致性约束,求解旋转矩阵 \mathbf{R} ,平移矩阵 \mathbf{T} 的 t_x , t_y 分量及尺度因子 s_x

具体步骤:

- •1) 令光心坐标 (u₀,v₀)为图像中心
- •2) 根据第*i*个标定像素点(*u_{di}*,*v_{di}*) 计算 (*x*["]_{di}, *y*["]_{di})

$$x_d'' = (u - u_0) d_x N_{cx} / f_{cx}$$
$$y_d'' = (v - v_0) d_y$$

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基于RAC的像机标定:第一步

•3) 根据其世界坐标(X_i, Y_i, Z_i), 列超定方程组, 求解 $a_1 \sim a_7$

$$\begin{bmatrix} X_{0}y_{d0}^{"} & Y_{0}y_{d0}^{"} & Z_{0}y_{d0}^{"} & y_{d0}^{"} & -X_{0}x_{d0}^{"} & -Y_{0}x_{d0}^{"} & -Z_{0}x_{d0}^{"} \end{bmatrix} \begin{bmatrix} a_{1} \\ a_{2} \end{bmatrix} \begin{bmatrix} x_{d0}^{"} \\ a_{2} \end{bmatrix} \begin{bmatrix} x_{d0}^{"} \\ x_{d0} \end{bmatrix} \\ \vdots \\ \vdots \\ x_{n}y_{dn}^{"} & Y_{n}y_{dn}^{"} & Z_{n}y_{dn}^{"} & y_{dn}^{"} & -X_{n}x_{dn}^{"} & -Y_{n}x_{dn}^{"} & -Z_{n}x_{dn}^{"} \end{bmatrix} \begin{bmatrix} a_{5} \\ a_{6} \\ a_{7} \end{bmatrix} \begin{bmatrix} \dots \\ x_{n}^{"} \\ \vdots \\ x_{n}^{"} \end{bmatrix}$$

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• 4) 计算 $|t_y| = (a_5^2 + a_6^2 + a_7^2)^{-1/2}$

• 推导:

$$\left(a_{5}^{2} + a_{6}^{2} + a_{7}^{2}\right)^{-1/2} = \left(\left(r_{21}/t_{y}\right)^{2} + \left(r_{22}/t_{y}\right)^{2} + \left(r_{23}/t_{y}\right)^{2}\right)^{-1/2}$$
$$= \left|t_{y}\right| \cdot \left(r_{21}^{2} + r_{22}^{2} + r_{23}^{2}\right)^{-1/2}$$

根据旋转矩阵**R**正交性约束 $r_{21}^2 + r_{22}^2 + r_{23}^2 = 1$ 即得证

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基于RAC的像机标定:第一步

• 5) 计算
$$s_x = \left(a_1^2 + a_2^2 + a_3^2\right)^{1/2} \left|t_y\right|$$

• 推导:

$$\left(a_1^2 + a_2^2 + a_3^2\right)^{1/2} = \left(\left(s_x r_{11}/t_y\right)^2 + \left(s_x r_{12}/t_y\right)^2 + \left(s_x r_{13}/t_y\right)^2\right)^{1/2} \\ = \left(\left(s_x/t_y\right)^2 \cdot \left(r_{11}^2 + r_{12}^2 + r_{13}^2\right)\right)^{1/2} = s_x/|t_y|$$

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• 6) 先假设 t_y符号为正, 计算 r₁₁~r₂₃和 t_x

$$\begin{aligned} r_{11} &= a_1 \cdot t_y / s_x = \left(s_x r_{11} / t_y \right) \cdot t_y / s_x & t_x = a_4 \cdot t_y / s_x = \left(s_x t_x / t_y \right) \cdot t_y / s_x \\ r_{12} &= a_2 \cdot t_y / s_x = \left(s_x r_{12} / t_y \right) \cdot t_y / s_x \\ r_{13} &= a_3 \cdot t_y / s_x = \left(s_x r_{13} / t_y \right) \cdot t_y / s_x \\ r_{21} &= a_5 \cdot t_y = \left(r_{21} / t_y \right) \cdot t_y \\ r_{22} &= a_6 \cdot t_y = \left(r_{22} / t_y \right) \cdot t_y \\ r_{23} &= a_7 \cdot t_y = \left(r_{23} / t_y \right) \cdot t_y \end{aligned}$$

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- •7)确定 t_y 符号
- •取任意一个标定点世界坐标(X_i, Y_i, Z_i),则可计算出其在像机坐标系下的坐标

 $x_{i} = r_{11}X_{i} + r_{12}Y_{i} + r_{13}Z_{i} + t_{x} \qquad y_{i} = r_{21}X_{i} + r_{22}Y_{i} + r_{23}Z_{i} + t_{y}$

• 根据对应图像投影点坐标 (u_i, v_i) ,则可计算图像投影点在像机坐标系下的坐标 $x'_{di} = s_x^{-1} (u_i - u_0) d_x N_{cx} / f_{cx}$ $y'_{di} = (v_i - v_0) d_y$

•实际像机系统中 x'_{di} 与 x_i 同号; y'_{di} 与 y_i 也为同号。若上述计算结果不满足同号约束,则 t_y 取负号。

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基于RAC的像机标定:第一步

•8) 根据旋转矩阵R的正交性,计算r₃₁, r₃₂, r₃₃

$$\begin{bmatrix} r_{31} \\ r_{32} \\ r_{33} \end{bmatrix} = \begin{bmatrix} r_{11} \\ r_{12} \\ r_{13} \end{bmatrix} \times \begin{bmatrix} r_{21} \\ r_{22} \\ r_{23} \end{bmatrix}$$
$$r_{31} = r_{12}r_{23} - r_{13}r_{22}$$
$$r_{31} = r_{12}r_{23} - r_{13}r_{22}$$
$$r_{32} = r_{13}r_{21} - r_{11}r_{23}$$

 $r_{33} = r_{11}r_{22} - r_{12}r_{21}$

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• 根据已求解的旋转矩阵**R**,平移矩阵**T**的 t_x , t_y 分量及尺度因子 s_x , 求解焦 距f, 平移矩阵**T**的 t_z 分量和径向畸变参数 k_1 。

• 带径向畸变参数 k₁的成像公式

$$\begin{cases} x'_{ui} = f \frac{x_i}{z_i} = f \frac{r_{11}X_i + r_{12}Y_i + r_{13}Z_i + t_x}{r_{31}X_i + r_{32}Y_i + r_{33}Z_i + t_z} \\ y'_{ui} = f \frac{y_i}{z_i} = f \frac{r_{21}X_i + r_{22}Y_i + r_{23}Z_i + t_y}{r_{31}X_i + r_{32}Y_i + r_{33}Z_i + t_z} \end{cases} \begin{cases} x'_{ui} = x'_{di} \left(1 + k_1 r_i^2 + k_2 r_i^2\right) \\ y'_{ui} = y'_{di} \left(1 + k_1 r_i^2 + k_2 r_i^2\right) \end{cases}$$

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•推导带径向畸变参数 k₁的成像公式(续)

 $\begin{cases} x'_{di} = s_x^{-1} (u_i - u_0) d_x N_{cx} / f_{cx} \\ y'_{di} = (v_i - v_0) d_y \end{cases}$

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- 具体步骤:
- •1) 不考虑畸变,即k₁=0,列超定方程组

$$y'_{d} = (v_{i} - v_{0})d_{y} = f \frac{r_{21}X_{i} + r_{22}Y_{i} + r_{23}Z_{i} + t_{y}}{r_{31}X_{i} + r_{32}Y_{i} + r_{33}Z_{i} + t_{z}}$$

$$\begin{bmatrix} \vdots \\ r_{21}X_i + r_{22}Y_i + r_{23}Z_i + t_y & -(v_i - v_0)d_y \end{bmatrix} \begin{bmatrix} f \\ t_z \end{bmatrix} = \begin{bmatrix} (v_i - v_0)d_y (r_{31}X_i + r_{32}Y_i + r_{33}Z_i) \\ \vdots \end{bmatrix}$$

采用线性最小二乘求解 $f和 t_z$

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- •2)估计*f、t_z和k*1真实值
 - 将k₁=0时得到的f和t_z作为非线性优化的初始值,采用采用非线性优化方法,解下列非线
 性方程,经优化搜索得到f、t_z和 k₁的精确解。

$$\begin{cases} x'_{d} + x'_{d}k_{1}\left(x'_{d}^{2} + y'_{d}^{2}\right) = f \frac{r_{11}X_{i} + r_{12}Y_{i} + r_{13}Z_{i} + t_{x}}{r_{31}X_{i} + r_{32}Y_{i} + r_{33}Z_{i} + t_{z}} \\ y'_{d} + y'_{d}k_{1}\left(x'_{d}^{2} + y'_{d}^{2}\right) = f \frac{r_{21}X_{i} + r_{22}Y_{i} + r_{23}Z_{i} + t_{y}}{r_{31}X_{i} + r_{32}Y_{i} + r_{33}Z_{i} + t_{z}} \end{cases}$$

<u>LM(Levenberg-Marquarelt)算法</u>

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第二讲 图像采集

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相机投影矩阵

$$z_{p} \begin{bmatrix} u \\ v \\ 1 \end{bmatrix} = \begin{bmatrix} f_{x} & 0 & u_{0} & 0 \\ 0 & f_{y} & v_{0} & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} \mathbf{R}_{3\times 3} & \mathbf{T}_{3\times 1} \\ \mathbf{0}_{3\times 1}^{T} & 1 \end{bmatrix} \begin{bmatrix} X \\ Y \\ Z \\ 1 \end{bmatrix}$$

$$z_{p}\begin{bmatrix} u\\v\\1\end{bmatrix} = \begin{bmatrix} f_{x} & \gamma & u_{0} & 0\\0 & f_{y} & v_{0} & 0\\0 & 0 & 1 & 0\end{bmatrix} \begin{bmatrix} \mathbf{R}_{3\times 3} & \mathbf{T}_{3\times 1}\\\mathbf{0}_{3\times 1}^{T} & 1\end{bmatrix} \begin{bmatrix} X\\Y\\\\Z\\1\end{bmatrix}$$

y表示u轴和v轴的不垂直因子。

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张正友平面标定思想

将世界坐标系原点位于平面标定板上(通常左上角)

世界坐标系X_wO_wY_w平面与标定板平面重合

标定板上的点其世界坐标**Z**_w=0



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相机投影矩阵



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相机坐标系<-->世界坐标系



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新的相机投影公式



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单应性矩阵

单应性(Homography):一个平面到另一个平面的投影映射

$$\begin{bmatrix} u \\ v \\ 1 \end{bmatrix} = \mathbf{H}_{3\times 3} \begin{bmatrix} X \\ Y \\ 1 \end{bmatrix}$$
$$\mathbf{H}_{3\times 3} = \begin{bmatrix} \mathbf{h}_1 & \mathbf{h}_2 & \mathbf{h}_3 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} & h_{13} \\ h_{21} & h_{22} & h_{23} \\ 0 & 0 & 1 \end{bmatrix}$$

一幅棋盘格平面图可以估计出一个单应性矩阵H。

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单应性矩阵→内参矩阵



计算内参矩阵 • 令 $\mathbf{B} = \mathbf{A}^{-T} \mathbf{A}^{-1} = \begin{bmatrix} B_{11} & B_{12} & B_{13} \\ B_{21} & B_{22} & B_{23} \\ B_{31} & B_{32} & B_{33} \end{bmatrix}$ B为对称阵,其有效元素为六个 • 定义 $\mathbf{b} = \begin{bmatrix} B_{11} & B_{12} & B_{22} & B_{13} & B_{23} & B_{33} \end{bmatrix}^T$ $h_i^T B h_j = v_{ij}^T b$ • 推导可得 $v_{ij} = [h_{i1}h_{j1} \quad h_{i1}h_{j2} + h_{i2}h_{j1} \quad h_{i2}h_{j2} \quad h_{i3}h_{j1} + h_{i1}h_{j3} \quad h_{i3}h_{j2} + h_{i2}h_{j3} \quad h_{i3}h_{i3}]^T$ 由约束条件可得 $\begin{bmatrix} v_{12}^T \\ (v_{12} - v_{12})^T \end{bmatrix} b = 0$

一幅棋盘格平面图可以列出2个等式,至少需要三幅棋盘格平面图估计出B。

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•一旦B被估计得到,可计算出相机内参

$$v_{0} = (B_{12}B_{13} - B_{11}B_{23}) / (B_{11}B_{22} - B_{12}^{2})$$

$$\lambda = B_{33} - [B_{13}^{2} + v_{0}(B_{12}B_{13} - B_{11}B_{23})] / B_{11}$$

$$\alpha = \sqrt{\lambda / B_{11}}$$

$$\beta = \sqrt{\lambda B_{11} / (B_{11}B_{22} - B_{12}^{2})}$$

$$\gamma = -B_{12}\alpha^{2}\beta / \lambda$$

$$u_{0} = \gamma v_{0} / \alpha - B_{13}\alpha^{2} / \lambda$$

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计算外参矩阵

 $r_{1} = \lambda A^{-1}h_{1}$ $r_{2} = \lambda A^{-1}h_{2}$ $r_{3} = r_{1} \times r_{2}$ $t = \lambda A^{-1}h_{3}$

•后续步骤(略):

(1)最大似然估计:由于上述推导结果是基于理想情况下的解,考虑到可能存在的高斯噪声,需使用最大似然估计进行优化。

(2) 径向畸变估计,类似Tasi方法

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标定方法(具体见程序操作)

http://robots.stanford.edu/cs223b04/JeanYvesCalib/index.html#links

Camera Calibration Toolbox for Matlab



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• Download the calibration images, and store the calibration images into a seperate folder named **calib_example**.



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• Run the main matlab calibration function **calib_gui** (or **calib**). A mode selection window appears on the screen:



• let us select the standard mode by clicking on the top button of the window. The main calibration toolbox window appears on the screen (replacing the mode selection window):

📣 Camera Calibration Toolbox - Standard Version			
lmage names	Read images	Extract grid corners	Calibration
Show Extrinsic	Reproject on images	Analyse error	Recomp. corners
Add/Suppress images	Save	Load	Exit
Comp. Extrinsic	Undistort image	Export calib data	Show calib results

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- Reading the images:
- Click on the Image names button in the Camera calibration tool window. Enter the basename of the calibration images (Image) and the image format (tif).
 - All the images (the 20 of them) are then loaded in memory (through the command **Read images** that is automatically executed) in the
 - variables **I_1**, **I_2**,..., **I_20**. The number of images is stored in the variable **n_ima (=20 here)**.

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The matlab window should look like this:

. Image11.tif Image15.tif Image19.tif Image4.tif Image8.tif .. Image12.tif Image16.tif Image2.tif Image5.tif Image9.tif Image13.tif Image17.tif Image20.tif Image6.tif Image10.tif Image14.tif Image18.tif Image3.tif Image7.tif

```
Basename camera calibration images (without number nor suffix): Image
Image format: ([]='r'='ras', 'b'='bmp', 't'='tif', 'p'='pgm', 'j'='jpg', 'm'='ppm') t
Loading image 1...2...3...4...5...6...7...8...9...10...11...12...13...14...15...16...17...18...19...20...
done
```

The complete set of images is also shown in thumbnail format



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• Extract the grid corners

Click on the Extract grid corners button in the Camera calibration tool window.

Extraction of the grid corners on the images Number(s) of image(s) to process ([] = all images) =

Press "enter" to select all the images. Then, select the default window size of the corner finder: wintx=winty=5 by pressing "enter" with empty arguments to the wintx and winty question. This leads to a effective window of size 11x11 pixels.

```
Extraction of the grid corners on the images

Number(s) of image(s) to process ([] = all images) =

Window size for corner finder (wintx and winty):

wintx ([] = 5) =

winty ([] = 5) =

Window size = 11x11

Do you want to use the automatic square counting mechanism (0=[]=default)

or do you always want to enter the number of squares manually (1,other)?
```

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• The corner extraction engine includes an automatic mechanism for counting the number of squares in the grid. In this present example, it is perfectly appropriate to keep working in the default mode (i.e. with automatic square counting activated), and therefore, simply press "enter" with an empty argument.

Do you want to use the automatic square counting mechanism (0=[]=default) or do you always want to enter the number of squares manually (1,other)?

```
Processing image 1...
Using (wintx,winty)=(5,5) - Window size = 11x11 (Note: To reset the window size, run script clearwin)
Click on the four extreme corners of the rectangular complete pattern (the first clicked corner is the origin)...
```

The first calibration image is then shown on Figure 2





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• Click on the four extreme corners on the rectangular checkerboard pattern. The clicking locations are shown on the four following figures.

Ordering rule for clicking: The first clicked point is selected to be associated to the origin point of the reference frame attached to the grid. The other three points of the rectangular grid can be clicked in any order. This first-click rule is especially important if you need to calibrate externally multiple cameras.



Click on the four extreme corners of the rectangular pattern (first corner = origin)... Image 1 Click on the four extreme corners of the rectangular pattern (first corner = origin)... Image 1





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• The boundary of the calibration grid is then shown on Figure 2:



Enter the sizes **dX** and **dY** in X and Y of each square in the grid (in this case, **dX=dY=30mm**=default values):

Size dX of each square along the X direction ([]=30mm) = 30 Size dY of each square along the Y direction ([]=30mm) = 30

Note that you could have just pressed "enter" with an empty argument to select the default values. The program automatically counts the number of squares in both dimensions, and shows the predicted grid corners in absence of distortion:



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• If the predicted corners are close to the real image corners, then the following step may be skipped. Press "enter", and the corners are automatically extracted using those positions as initial guess.

The image corners are then automatically extracted, and displayed on figure 3 (the blue squares around the corner points show the limits of the corner finder window):



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The corners are extracted to an accuracy of about 0.1 pixel.
Follow the same procedure for the 2nd, 3rd, ... images. For example, here are the detected corners of image 2, 3, 4, 5, 6 and 7:



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• Main Calibration step

After corner extraction, click on the button **Calibration** of the **Camera calibration tool** to run the main camera calibration procedure.

Calibration is done in two steps: first initialization, and then nonlinear optimization.

The initialization step computes a closed-form solution for the calibration parameters based not including any lens distortion (program name: **init_calib_param.m**).

The non-linear optimization step minimizes the total reprojection error (in the least squares sense) over all the calibration parameters (9 DOF for intrinsic: focal, principal point, distortion coefficients, and 6*20 DOF extrinsic => 129 parameters).

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Aspect ratio optimized (est_aspect_ratio = 1) -> both components of fc are estimated (DEFAULT). Principal point optimized (center_optim=1) - (DEFAULT). To reject principal point, set center_optim=0 Skew not optimized (est_alpha=0) - (DEFAULT) Distortion not fully estimated (defined by the variable est_dist): Sixth order distortion not estimated (est_dist(5)=0) - (DEFAULT) . Initialization of the principal point at the center of the image. Initialization of the image distortion to zero. Initialization of the intrinsic parameters using the vanishing points of planar patterns.

Initialization of the intrinsic parameters - Number of images: 20

Calibration parameters after initialization:

 Focal Length:
 fc = [671.13759
 680.77186]

 Principal point:
 cc = [319.50000
 239.50000]

 Skew:
 alpha_c = [0.00000]
 => angle of pixel = 90.00000 degrees

 Distortion:
 kc = [0.00000
 0.00000
 0.00000
 0.00000

Main calibration optimization procedure - Number of images: 20 Gradient descent iterations: 1...2...3...4...5...6...7...8...9...10...11...done Estimation of uncertainties...done

Calibration results after optimization (with uncertainties):

```
      Focal Length:
      fc = [ 661.67001 662.82858 ] ± [ 1.17913 1.26567 ]

      Principal point:
      cc = [ 306.09590 240.78987 ] ± [ 2.38443 2.17481 ]

      Skew:
      alpha_c = [ 0.00000 ] ± [ 0.00000 ] => angle of pixel axes = 90.00000 ± 0.00000 degrees

      Distortion:
      kc = [ -0.26425 0.22645 0.00020 0.00023 0.00000 ] ± [ 0.00934 0.03826 0.00052 0.00053 0.00000 ]

      Pixel error:
      err = [ 0.45330 0.38916 ]
```

Note: The numerical errors are approximately three times the standard deviations (for reference).

Recommendation: Some distortion coefficients are found equal to zero (within their uncertainties). To reject them from the optimization set est_dist=[1;1;0;0;0] and run Calibration

• On this figure, every camera position and orientation is represented by a green pyramid. Another click on the **Switch to camera-centered view** button turns the figure back to the "camera-centered" plot.



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第三章 图像采集

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习题3.1 P55

• 用一个带50mm焦距镜头的像机拍摄距离10m外,高2m的物体,该物体成像尺寸为多少?如果换为 135mm的镜头,成像尺寸为多少?



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习题3.1 P55

•1、已知物距*z*=10m,物高*y*=2m,焦距*f*=50mm

• 根据
$$\frac{1}{z'} + \frac{1}{z} = \frac{1}{f}$$
 , 有 $\frac{1}{z'} + \frac{1}{10} = \frac{1}{0.05} \Rightarrow z' \approx 0.05025 \text{ m}$

•2、已知物距*z*=10m,物高*y*=2m,焦距*f*=135mm

$$\frac{1}{z'} + \frac{1}{10} = \frac{1}{0.135} \Longrightarrow z' \approx 0.13685 \text{ m} \qquad y' = 0.13685 \times \frac{2}{10} = 0.02737 \text{ m}$$

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习题3.6 P56

- 设图像的长宽比为4:3,进行以下计算
 - •100万像素手机拍摄的图像空间分辨率约为多少?
 - •1000万像素像机拍摄的图像空间分辨率约为多少?它拍摄的一幅彩色图像需多少字节来存储。
- •解:设图像宽度 w,则高度h=3w/4,图像大小为:

 $w \cdot 3w/4 = 1,000,000 \implies w \approx 1154, h \approx 866$ $w \approx 3651, h \approx 2738$

若是1000万像素的像机,则

•彩色图像1个像素需3个字节,1000万像素即需3000万个字节,即30MB

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习题3.6 P56

常用分辨率: 640×480 约为30万像素

1024×768约为80万像素

1280×960约为130万像素(1.3M)

1600×1200约为200万像素(2M)

若长宽比为16:9

1280×720约为100万像素(720P)

1920×1080约为200万像素(1080i/1080P)

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